

**SYSTEM AND METHOD OF BATTERY CAPACITY ESTIMATION****CROSS-REFERENCE TO RELATED APPLICATION**

This application claims the benefit of United States Provisional Application Serial No.

5 60/412,744, filed on September 24, 2002, the entire disclosure of which is incorporated herein  
by reference.

**FIELD**

10 The technology described in this patent document relates generally to the field of  
battery-powered devices. More particularly, this patent document relates to techniques of  
battery capacity estimation.

**BACKGROUND**

15 Mobile communication devices, such as cellular telephones, two-way pagers and  
others typically rely on power from batteries. It is, therefore, advantageous for a mobile  
communication device to monitor the amount of time remaining before the device loses power  
due to a drained battery. For example, a mobile communication device may issue a warning  
signal during a call to avoid an imminent shut-off when the battery output drops below a  
particular threshold. Typical cellular service provides a three to five minute low-battery  
20 warning period during a call and similar warnings when the device is idle.

Mobile communication devices typically measure battery capacity in units of current  
multiplied by time, such as milliamp hours (mAh). However, direct current measurement may  
not be available in certain devices. In addition, the variation of battery parameters, such as  
temperature, equivalent series resistance (ESR), and aging, often make it difficult for a device  
25 to perform an accurate prediction. The multi-mode operations available in some devices (e.g.,  
sleep, wake-up, access, traffic) may make this estimation even more difficult.

**SUMMARY**

Systems and methods are provided for battery capacity estimation. A profile table may be used that relates a plurality of battery profile values with a plurality of operating parameter values. The profile table may be accessed to translate one or more measured operating parameters into one or more corresponding battery profile values. One or more of the battery profile values may be adjusted by a correction factor to generate a corrected battery profile value. The available capacity of the battery may be calculated using the corrected battery profile value. The correction factor may then be automatically calibrated using an estimated battery profile value calculated from the one or more measured operating parameters. In addition, the following method steps may be performed. Determining an equivalent series resistance value for the battery. Determining a load voltage value for the battery. Determining a load current value for the battery. Determining the unloaded voltage value as a function of the equivalent series resistance value, the load voltage value, and the load current value.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

Fig. 1 is a block diagram of an example mobile communication device;

Fig. 2 is an example battery measurement subsystem for a mobile communication device;

Fig. 3 is a flowchart of an example battery capacity processing method;

Fig. 4 is a flowchart of an example method for selecting a battery profile;

Fig. 5 is a flowchart illustrating an example method for sampling battery measurements;

Fig. 6 is a flowchart illustrating an example method for battery measurement preprocessing;

Fig. 7 is a flowchart illustrating example battery measurement, preprocessing, and capacity-processing methods;

Fig. 8 is a flowchart illustrating an example self-calibration method;

Fig. 9 is a flowchart illustrating an example method for the self-calibration of the ESR compensation factor in Fig. 8;

Fig. 10 is a flowchart illustrating another self-calibration method;

Fig. 11 is a flowchart illustrating an example method for the self-calibration of the capacity compensation factor in Fig. 10; and

Fig. 12 is a flowchart illustrating an example of the actions step shown in Fig. 3.

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### **DETAILED DESCRIPTION**

Fig. 1 is a block diagram of an example mobile communication device 110. The mobile communication device 110 includes a transceiver 111 for communicating data signals with a base station antenna 119. The data signals may be voice, information at different data rates, or other types of signals, both digital and analog.

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The base station antenna 119 may be part of an analog or digital cellular network or some other type of data network. The voice and data networks may be separate communication networks using separate infrastructure, such as base stations or network controllers, or they may be integrated into a single wireless network.

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In one embodiment, the transceiver 111 includes a receiver 112, a transmitter 114, one or more local oscillators 113, a digital signal processor (DSP) 120, and transmit and receive antennas 116, 118. In another embodiment, the transceiver uses a single antenna to which the transmitter and receiver are diplexed.

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The DSP 120 sends and receives data signals to and from the transmitter 114 and receiver 112. The DSP 120 also receives control information from the transmitter 114 and the receiver 112 and provides control information to the transmitter 114 and the receiver 112.

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A single local oscillator 113 may be used in conjunction with the transmitter 114 and receiver 112 if the voice and data communications occur at a single frequency or a closely spaced set of frequencies. Alternatively, if different frequencies are utilized for voice communications versus data communications, then a plurality of local oscillators 113 can be used to generate multiple frequencies corresponding to the voice and data networks 119.

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A microprocessor 138 controls the operation of the mobile device 110. It should be understood, however, that other embodiments may include micro-controllers, DSPs, or other types of processing devices. A display 122 (e.g., LCD, LED) provides the microprocessor with the ability to display information to a user.

The mobile communication device 110 has memory for temporarily and/or permanently storing data. The memory includes flash memory 124 and random access

memory (RAM) 126, but could include other types of memory, such as semiconductor memory (e.g., ROM), magnetic, optical or others. The memory can be used to store data, such as the mobile device's operating system, operational data, user preferences, temporary data from the microprocessor 138, or other types of data.

5           In one embodiment, the flash memory 124 stores a plurality of software application modules 124A - 124N that can be executed by the microprocessor 138, the DSP 120, and/or another processing device. The application modules include a voice communication module 124A, a data communication module 124B, and a plurality of other operational modules 124N for carrying out other functions. The battery capacity estimation program described herein  
10       may, for example, be stored in the flash memory 124, but could be stored in other permanent memory (e.g., ROM) in the mobile communication device 110.

          Additional application modules 124N may be loaded onto the device 110 through the network 119, through an auxiliary I/O subsystem 128, through the serial port 130, through the short-range communications subsystem 140, or through another suitable subsystem 142, and  
15       installed by a user in the Flash memory 124 or RAM 126. Such flexibility in application installation increases the functionality of the device 110 and may provide enhanced on-device functions, communication-related functions, or both. For example, various parameters and/or steps of the battery capacity estimation program, described below, may be updated in this manner.

20           The mobile device includes auxiliary input/output (I/O) devices 128, a serial port and/or a USB130, a keyboard 132, a speaker 134, and a microphone 136 to enable access to the operation of the device.

          A short-range wireless communications sub-system 140 and other device sub-systems 142, are also included in the mobile communication device 110. The short-range  
25       communications subsystem 140 may include an infrared device and associated circuits and components, or a BLUETOOTH short-range wireless communication module to provide communication with similarly enabled systems and devices. Other device sub-systems 142 may include battery condition measurement circuitry, as described below.

          Fig. 2 illustrates an example battery measurement subsystem 200 for a mobile  
30       communication device. The battery measurement subsystem 200 may, for example, be one of the other device subsystems 142 illustrated in Fig. 1.

The battery measurement subsystem 200 may receive a selection command from the microprocessor 138 and send a measurement value (i.e., a value indicating the battery state) to the microprocessor 138 in response to the selection command.

5 The battery measurement subsystem 200 includes a battery pack 210 that powers the mobile device 110 of Fig. 1. The battery pack 210 includes a cell 212, a battery temperature sensor 214, and an identification block 216. The identification block 216 may enable the microprocessor 138 to determine the type of battery 210.

10 The battery temperature sensor 214 provides a battery temperature signal that indicates the temperature of the battery pack 210. The battery temperature signal is conditioned by the battery temperature signal conditioning block 224 to generate the signal  $T_{bat}$ . The signal conditioning block 224 performs typical conditioning functions, such as filtering, scaling and/or amplifying. The signal conditioning block 224 may also perform other functions, such as providing bias required by the identification unit 216, multiplexer 240 and/or the analog to digital converter 250. The  $T_{bat}$  signal is coupled to an input of the multiplexer 240 for  
15 selection by the microprocessor 138.

The voltage and current of the cell 212 is monitored by the cell signal conditioning block 222. The cell signal conditioning block 222 provides a conditioned battery voltage signal,  $V_{out+}$ , and a conditioned battery current signal,  $I_1$ , to the inputs of the multiplexer 240 for selection by the microprocessor 138.

20 In one alternate embodiment, the cell signal conditioning block 222 may not provide a battery current. In this case, the current may be obtained indirectly by measuring TX power and by detecting other device states that affect current, such as operation of backlight, buzzer and LED (within the other devices subsystem 142), as described below.

25 The TX power sensor 242 detects the transmit power of the transmitter 114 (Fig. 1), and inputs the transmit power to the TX power signal conditioning block 232. The TX power conditioning block 232 performs typical conditioning functions, such as filtering, scaling or amplifying, as well as providing a bias that may be required by the Tx power sensor 242, multiplexer 240 and/or the analog to digital converter 250. The Tx power conditioning block 232 generates the  $TX_p$  signal that is coupled to the multiplexer 240 for selection by the  
30 microprocessor 138.

The incremental current consumption of the additional devices, such as backlight, buzzer and LED within the other devices subsystem 142, are pre-characterized and their values are stored in flash memory 124 according to the states of these devices. The software that runs on the microprocessor 138 controls the operation of these device states and, therefore, the states can be detected and corresponding incremental current consumptions by these devices can be included in the processing.

A board temperature sensor 244 provides a board temperature signal, Tbrd, that indicates the temperature of the printed circuit board of the transceiver 111 of Fig. 1. This signal is conditioned by the board temperature signal conditioning block 234 and coupled to an input of the multiplexer 240.

The identification block 216, provides the identification signal Battery ID that is conditioned by the identification signal conditioning block 226 and input to the multiplexer 240.

In operation, multiplexer 240 responds to the selection signal sent by the microprocessor 138 to drive a select measurement signal such as: Tbrd, Vout+, I1, TXp, Tbat or the battery ID, through the analog to digital converter 250. The analog to digital converter 250 digitizes the signal output from the multiplexer 240 and sends the digital representation of the measurement value to the microprocessor 138. For example, if the microprocessor 138 requests a battery ID, a predetermined selection command assigned to the battery ID is transmitted to the multiplexer 240 of the battery measurement subsystem 200. The multiplexer 240 may use this command to switch the battery ID input to the output of the subsystem 200.

Fig. 3 includes a flowchart of an example battery capacity estimation method. A program for performing this method may, for example, be included in one of the software modules 124N illustrated in Fig. 1.

The illustrated other software module block 124N includes a battery capacity estimation software module 124C. The battery capacity estimation software module 124C is illustrated by flowchart 300. Also shown are multiple battery profiles 330A-330N that are stored with the software module 124C in flash memory 124, as well as pre-determined actions 360 that can be triggered by the battery capacity estimation software module 124C.

Battery profiles 1-N (330A-330N) support up to N battery packs 210 that a user may plug in and use on the mobile unit 110. Each battery profile 330A-330N identifies a given battery pack. In other words, for a specific battery pack 210 there corresponds a specific battery profile 330.

5 As described below, values of some of the tables in the profiles 330A-330N are dependent on the maker/model/version/batch of the battery pack, their values are determined at the time of battery manufacture and are loaded into the corresponding tables in 330A-330N. Values of other tables in the profiles 330A-330N are specific to a battery pack. A further description of these values is provided below.

10 Each battery profile 330A-330N may include multiple tables that profile a particular battery. These tables may include the Equivalent Series Resistance (ESR) versus battery temperature (Tbat) 332, the current (I) versus transmit power (TXP) 334, the battery voltage threshold value at which the radio shuts off (VROFF) stored as a function of board temperature (Tbrd) 336, the battery capacity (CAP) as a function of unloaded voltage (V) 338,  
15 the battery capacity compensation factor at temperature Tbat 340, and the ESR compensation factor at temperature Tbat 342. This is illustrated as Profile 1 330A through Profile N of Fig. 3.

In another embodiment, I\_VS\_TXP and VROFF\_VS\_T may be determined by the transceiver and not the battery. In such an embodiment, these values may not be part of the  
20 battery profile.

In operation, at step 310 the method samples the battery measurements that include various operating parameters of the battery, such as temperature (T), loaded voltage (V\_load), current (I<sub>l</sub>), and transmit power (TX<sub>p</sub>). When the method is used in co-operation with the subsystem of Fig. 2, this step may include instructing the microprocessor 138 to send at least  
25 one selection signal to the multiplexer 240 of the battery measurement subsystem 200. The microprocessor 138 then reads the selected measurement for each selection signal sent at the output of the analog to digital converter 250.

At step 320, the battery measurements sampled at step 310 are pre-processed to provide intermediate results used in the battery capacity processing step 350. In  
30 preprocessing, at least one of the multiple battery profiles 330A-N is used to translate the measurement to a corresponding value (e.g., temperature to resistance).

With reference to Profile 1 330A, the intermediate results from the pre-processing step 320 may include:

1) The ESR\_VS\_T 332A table translates the temperature to resistance through linear interpolation in the battery capacity estimation method. The table size may, for example, be eight elements that are equally spaced between -20° to 75° C, unsigned. This interpolation can be expressed by:

$$\text{ESR}(\text{Tbat}) = \text{Linear\_interpolate}(\text{ESR\_VS\_T}, \text{Tbat});$$

where Linear\_interpolate (ESR\_VS\_T, Tbat) represents the linear interpolation of the table ESR\_VS\_T at temperature Tbat.

The values stored in the table are the average values obtained by characterization of the battery pack upon manufacture.

2) The I\_VS\_TXP 334A table translates the transmit power to current through linear interpolation. This can be expressed by:

$$\text{I}(\text{TXp}) = \text{Linear\_interpolate}(\text{I\_VS\_TXP}, \text{TXp});$$

where Linear\_interpolate (I\_VS\_TXP, TXp) represents the linear interpolation of the table I\_VS\_TXP at transmit power TXp.

The values stored in the table are obtained by characterizing the current consumption of the entire device 110, which includes transmit power characteristics of the transceiver 111 of Fig. 1. This table translates the transmit power to current through linear interpolation. For example, the transmit power can be sensed by the transmit power sensor 242 of Fig. 2. Alternatively, the transmit power can be read from the transmit automatic gain control (AGC) or equivalent. Averaging of the translated current value can be used to obtain a more stable result. The battery current may further include other device consumptions, such as buzzer, backlight and LED, that are pre-characterized and stored in flash memory. The state of these devices detected by software running in the microprocessor 138 determines the value of the additional current.

In another embodiment, if current I1 is directly available via cell signal conditioning 222 of Fig. 2, then the table I\_VS\_TXP 334A and the above intermediate result may not be needed. In this case, battery current is obtained directly by measuring I1.

3) The VROFF\_VS\_T 336A table is made up of an array of the battery voltage threshold values at which the radio shuts off as a function of board temperature. In one



embodiment, the elements are equally spaced over the temperature range of -20° to 75° C. The threshold value at a given temperature, Tbrd, is calculated by linear interpolation of the elements in the array. This interpolation can be expressed as:

$$V\_roff(Tbrd) = \text{Linear\_interpolate}(VROFF\_VS\_T, Tbrd);$$

5        where Linear\_interpolate (VROFF\_VS\_T, Tbrd) represents the linear interpolation of the table VROFF\_VS\_T at board temperature Tbrd.

4)        The loaded battery voltage is monitored periodically during a call and periodically during standby. During standby, the measured voltage may be treated as an unloaded voltage. During a call, the measured loaded voltage is translated to the unloaded  
10        voltage using the equation:

$$V = V\_load + I\_battery \cdot F\_esr(Tbat) \cdot ESR(Tbat);$$

where V is the translated unloaded voltage and V\_load is the measured voltage during the call. In one embodiment, the measured voltage may be obtained by selecting the “Vout+” multiplexer 240 input provided by the cell signal conditioning block 222 of Fig. 2.

15        I\_battery may be equal to I(TXp) + I(state), wherein I(TXp) is the translated current based on the table given in 2) above, and the I(state) is the total incremental current consumption of additional devices (such as buzzer, backlight and LED) that is pre-characterized and stored in a flash memory. The device state that determines I(state) may be detected by the software.

20        Alternatively I\_battery may be obtained by selecting the “I1” multiplexer 240 input provided by the cell signal conditioning block 222 of Fig. 2. The V\_load and I\_battery may be measured effectively at the same time. ESR(Tbat) is the interpolated value obtained as described previously. F\_esr(Tbat) is a self-calibrating correction factor at the temperature Tbat that is detailed below in relation to the self-calibration of stored values FESR\_VS\_T  
25        342A in step 370. F\_esr(Tbat) • ESR(Tbat) together represents the translated and corrected ESR.

During standby, V is the battery voltage value. This may be obtained by selecting the “Vout+” multiplexer 240 input provided by the cell signal conditioning block 222 of Fig. 2.

5)        The battery capacity as a function of unloaded voltage may be characterized at  
30        manufacture and stored in the table CAP\_VS\_V 338A of Fig. 3 as elements that are equally

spaced over a predetermined voltage range of 2.9000 – 4.5384V. The capacity at unloaded voltage V is obtained by linear interpolation by the equation:

$$C\_model(V) = \text{Linear\_interpolate}(\text{CAP\_VS\_V}, V);$$

where V is the unloaded battery voltage, obtained by the calculation given in 4) above and Linear\_interpolate (CAP\_VS\_V, V) represents the linear interpolation of the table CAP\_VS\_V at voltage V.

The battery capacity processing 350 takes place using the intermediate results of the above-described preprocessing step 320. The battery capacity of the mobile device is estimated by:

$$C\_user(V, T_{bat}) = F\_cap(T_{bat}) \cdot C\_model(V);$$

where F\_cap(Tbat) is a self-calibrating correction factor at the temperature Tbat that is detailed below in relation to the self-calibration of stored values FCAP\_VS\_V 340A in step 370.

Various predetermined actions 360 may result from triggers that are dependent on the value of the battery capacity processing 350. These actions 360 may, for example, include warning messages displayed on the mobile device's display and shutting off the mobile device. Each of the actions 360 may be triggered by different values of estimated battery capacity, or measured voltage. Alternate embodiments may have different actions for various values of estimated battery capacity. A flowchart illustrating one example action 360 is shown in Fig. 12, described below

After the battery capacity processing step 350, self-calibration of the correction factors occur at step 370. Since the FCAP\_VS\_T or FESR\_VS\_T initial values represent an average, freshly manufactured battery when they work with the CAP\_VS\_V or ESR\_VS\_T respectively, these values should be corrected to account for effects, such as battery aging, differences between battery packs, or other errors. The self-calibration includes self-calibration of the correction factors F\_esr(Tbat) and F\_cap(Tbat) of step 350.

The battery capacity may be used to identify a need for charging the battery or as an indication of the amount of time before the battery is discharged. While the battery discharges, the device monitors the voltage. The first critical value, V\_roff(Tbrd), is the one beyond which the radio ceases to perform within its specifications, and is dependant on temperature. Past the V\_roff(Tbrd), the radio portion of the hardware is turned off.

Further discharge, with the radio off, may bring the device to a second threshold,  $V_{dvo\text{ff}}$ . When  $V_{dvo\text{ff}}$  is reached, the device shuts off.

If battery capacity is assumed to be a function of unloaded voltage, then a full capacity is achieved when the unloaded voltage reaches the maximum battery voltage. “Available capacity” assumes that a “0” capacity is reached when the loaded voltage equals  $V_{dvo\text{ff}}$ . In order to make available capacity independent of device usage, a negligible current is assumed. “Assessible capacity” assumes that a “0” capacity is reached when the loaded voltage reaches  $V_{roff}(T_{brd})$  since the capacity is a function of unloaded voltage:

$$V_{roff\_unloaded}(T_{brd}) = V_{roff}(T_{brd}) + I_{\text{battery}} \cdot F_{\text{esr}}(T_{bat}) \cdot ESR(T_{bat});$$

where  $I_{\text{battery}}$  is the current delivered by the battery at the time of the capacity estimation,  $ESR(T_{bat})$  is the equivalent series resistance of the battery, and  $F_{\text{esr}}(T_{bat})$  is a self-calibrating correction factor at the temperature  $T_{bat}$  required to fine tune the equivalent series resistance of the battery.

It can be seen that the “0” capacity varies with the  $F_{\text{esr}}(T_{bat}) \cdot ESR(T_{bat})$  and with the device current. That is, “accessible capacity” represents a battery capacity that is based on current conditions.

When accessible capacity reaches “0”, the device ceases to perform within its specifications and will shut down the radio portion of the hardware. The user can then refer to the available capacity to decide when to charge the device. The accessible capacity may be referred to in order to estimate how much more usage the user can get out of the device.

In contrast to the available capacity that gradually decreases while in-use and increases while in the charger, the accessible capacity is highly dependant on external factors such as temperature and RF conditions. Therefore, the capacity of a battery is determined in a best-case scenario: the least current draw at room temperature. The availability of battery capacity is determined with an operational current draw and at a current temperature.

Because of various types of batteries on the market, it may be desirable to display the battery capacity in percentages of the maximum battery capacity. Therefore, the display may be calculated as follows:

$$\begin{aligned} C_{\text{available}} &= (C_{\text{user}}(V_{\text{now}}) - C_{\text{user}}(V_{dvo\text{ff}})) / \\ & (C_{\text{user}}(V_{\text{charged}}) - C_{\text{user}}(V_{dvo\text{ff}})); \\ C_{\text{accessible}} &= (C_{\text{user}}(V_{\text{now}}) - C_{\text{user}}(V_{roff\_unloaded}(T_{brd}))) / \end{aligned}$$

$(C_{\text{user}}(V_{\text{charged}}) - C_{\text{user}}(V_{\text{dloff}}));$

where  $V_{\text{now}}$  is the current unloaded voltage. Because of the continuous current draw,  $V_{\text{now}}$  should be calculated from the measured voltage and from the battery current:

$V_{\text{now}} = V_{\text{measured}} + I_{\text{battery}} \cdot F_{\text{esr}}(T_{\text{bat}}) \cdot \text{ESR}(T_{\text{bat}}).$

5  $V_{\text{roff\_unloaded}}(T_{\text{brd}})$  is the radio off unloaded voltage:

$V_{\text{roff\_unloaded}}(T_{\text{brd}}) = V_{\text{roff}}(T_{\text{brd}}) + I_{\text{battery}} \cdot F_{\text{esr}}(T_{\text{bat}}) \cdot \text{ESR}(T_{\text{bat}}).$

$V_{\text{measured}}$  is the measured voltage,  $I_{\text{battery}}$  is the current delivered by the battery measured simultaneously with  $V_{\text{measured}}$ , and  $V_{\text{charged}}$  is the voltage when the battery is fully charged. In one embodiment,  $V_{\text{charged}}$  is 4.2V.  $V_{\text{dloff}}$  is the battery voltage when  
10 the device shuts off. In one embodiment,  $V_{\text{dloff}}$  is 3.1V.

There can be different ways to display the available and the accessible capacity. One example is a battery picture. The available capacity may be displayed in gray. When the battery is charged, the battery picture will be completely filled. The accessible capacity may be displayed in black over the available capacity. Under ideal conditions, the two capacities  
15 will be close together with the accessible capacity slightly lower than the available capacity.

Messages to increase battery capacity may also be displayed. For example, if the radio is currently experiencing less than maximum received signal strength, a message could be displayed advising the user to move to another location to increase battery capacity. Similarly, if the measured temperature is lower than a predetermined temperature threshold (e.g., room  
20 temperature), a message could be displayed advising the user to warm the radio to increase capacity. Alternate embodiments use other criteria for determining when to display a message to increase battery capacity.

One embodiment of the ESR Estimation/Self-Calibration method is described subsequently as it relates to a mobile communication device capable of making and receiving  
25 radiotelephone or telephone calls. Alternate embodiments of this method include any mobile device that has a high use period and a stand-by state. The transmission period and stand-by state of a mobile communication device is only one such example.

An example of the ESR Estimation/Self-Calibration method illustrated in Fig. 3 is as follows. During a call, the temperature  $T$ , loaded voltage  $V_{\text{load}}$ , and current  $I_{\text{battery}}$  are  
30 periodically measured and stored, for instance in the RAM 126 of Fig. 1. After the call

termination and before the temperature noticeably changes, the loaded voltage  $V$  is measured again. An estimation of ESR can then be calculated by the equation:

$$\text{ESR}_{\text{estimated}}(T_{\text{bat}}) = (V_{\text{idle}} - V_{\text{load}}) / (I_{\text{battery}} - I_0);$$

5 where  $V_{\text{idle}}$  is the voltage measured after call termination,  $V_{\text{load}}$  is the latest voltage measurement before call termination,  $I_{\text{battery}}$  is the latest current measurement obtained at the same time as  $V_{\text{load}}$ ,  $I_0$  is a characterized value of current at idle state, stored ( $I_0$  may be in a flash memory or, alternatively, may be approximated by value zero), and  $T_{\text{bat}}$  is the measured battery temperature.

10 In calculating  $\text{ESR}_{\text{estimated}}(T_{\text{bat}})$ , the voltage and current should be measured effectively at the same time. Although the above description reads values into the microprocessor 138 sequentially, the voltage and current values can still be taken at the same time. For example, the cell signal conditioning 222 block may include a delay difference  $\Delta T$  between the  $V_{\text{out+}}$  branch and the  $I_1$  branch. When the selection signal commands the multiplexer 240, the commands between the voltage and current reading are separated by time  
15 difference  $\Delta T$ . The same method can also be used between the cell signal conditioning 222 for voltage and TX power signal conditioning 232 for  $\text{TXp}$  to convert to  $I(\text{TXp})$ , as well as the  $I(\text{state})$  for the states of other devices. Alternatively, one single command may be sent to sample and hold the voltage  $V_{\text{out+}}$  and current  $I_1$  (or Tx power  $\text{TXp}$ ) pair at cell signal conditioning 222 and TX power conditioning 232 at the same time instant. Yet another  
20 alternate is to design the signal conditioning blocks for voltage and current with the same delay, and utilize a two channel analog to digital converter to sample the voltage  $V_{\text{out+}}$  and current  $I_1$  (or  $\text{TXp}$ ) at the same time and fetch the values to the microprocessor 138 one after another.

25 The ESR can then be self-calibrated by defining the function  $F_{\text{esr}}(T_{\text{bat}})$  as an ESR correction factor at temperature  $T_{\text{bat}}$ . The  $F_{\text{esr}}(T_{\text{bat}})$  function may, for example, be stored in an array  $[F_1, F_2, \dots, F_n]$ , such as table  $\text{FESR\_VS\_T}$ . Each element of the array is the value of  $F_{\text{esr}}(T)$  at  $n$  temperatures  $T=T_1, T_2, \dots, T_n$ , spanning a temperature range of interest.

The value of  $F_{\text{esr}}(T_{\text{bat}})$  for temperature  $T_{\text{bat}}$  between any of the  $n$  temperature points is represented by the interpolated value of the adjacent element values. Initial values stored in  
30 table  $\text{FESR\_VS\_T}$  for  $F_1, F_2, \dots, F_n$  are all 1.0's. The value of the entry in the table

FESR\_VS\_T (342A) having a corresponding temperature that is closest to Tbat is updated by the value  $F_{\text{esr}}^{(\text{new})}(\text{Tbat})$ , which may be calculated as follows:

$$F_{\text{esr}}^{(\text{new})}(\text{Tbat}) = F_{\text{esr}}^{(\text{old})}(\text{Tbat}) + \beta \cdot \{ \text{ESRestimated}(\text{Tbat}) / \text{ESR}(\text{Tbat}) - F_{\text{esr}}^{(\text{old})}(\text{Tbat}) \};$$

5           where Tbat is the measured temperature, ESRestimated(Tbat) is generated as described above, ESR(Tbat) is interpolated from the table ESR\_VS\_T as described above,  $F_{\text{esr}}^{(\text{old})}(\text{Tbat})$  is the interpolated value from the table FESR\_VS\_T at temperature Tbat before the table is updated, and  $\beta$  is a small value that is used for iterative correction and may vary for each application.

10           Alternatively, the value in table FESR\_VS\_T may be reduced to only one element that is not a function of temperature, and corrections to ESR may be made using the single factor  $F_{\text{esr}}$  for any temperature. It should be understood, however, that using one factor to update the entire table is based on an approximation in which the “shape” of the characterized ESR does not noticeably change from device to device or by aging, but may proportionally vary. In  
15 this case, the following equations may be applied:

$$V = V_{\text{load}} + I_{\text{battery}} \cdot F_{\text{esr}} \cdot \text{ESR}(\text{Tbat});$$

$$F_{\text{esr}}^{(\text{new})} = F_{\text{esr}}^{(\text{old})} + \beta \cdot \{ \text{ESRestimated}(\text{Tbat}) / \text{ESR}(\text{Tbat}) - F_{\text{esr}}^{(\text{old})} \}$$

The self-calibrating correction factor  $F_{\text{cap}}(\text{Tbat})$ , as stated in reference to step 350 above, is used to correct the capacity model stored in table CAP\_VS\_V 338A.  $F_{\text{cap}}(\text{Tbat})$   
20 may be produced and updated as follows:

1)       The function  $F_{\text{cap}}(\text{Tbat})$  is a correction factor at temperature Tbat. This function is stored in an array form [F1, F2, ..., Fn], such as table FCAP\_VS\_T 340A, where each element is the value of  $F_{\text{cap}}(\text{Tbat})$  at n temperatures  $\text{Tbat} = \text{T1}, \text{T2}, \dots, \text{Tn}$ , spanning a predefined temperature range of interest. The value of  $F_{\text{cap}}(\text{Tbat})$  for temperature Tbat  
25 between any of the n temperature points is represented by the interpolated value of the adjacent element values. Initial values stored in table FCAP\_VS\_T for F1, F2, ..., Fn are all 1.0's.

2)       When a “battery low” warning message is given, the current  $I_{\text{battery}}$  is monitored periodically and more frequently at intervals of  $\Delta t$ . An accumulator accumulates  
30 the values of  $I_{\text{battery}}$  obtained at every interval  $\Delta t$ .

3) If the user does not terminate the call prior to the voltage dropping below a threshold, then the radio shut-off action occurs. This shut-off action is triggered by the first occurrence of  $V_{load} < V_{roff}(T_{brd})$ . Otherwise, the user terminates the call after the battery low warning and before the radio shut off action is triggered. In either case, the following functions may be performed:

a) Stop the current accumulator at the time the radio is turned off (by user or automatically), obtain the last value of  $\Sigma I_{battery}$ , and calculate the actual capacity change during the period from the low battery warning to the radio shut off as:  $\Delta C_{actual} = t \cdot \Sigma I_{battery}$ ;

b) Calculate the battery capacity model estimated capacity change before correction as:  $\Delta C_{est} = C_{model}(V_{warn}) - C_{model}(V_{idle})$ ; where  $V_{warn}$  is the unloaded voltage converted from loaded voltage at the time radio battery low warning message was issued; and  $V_{idle}$  is the unloaded voltage converted from the loaded voltage obtained after the radio is turned off (either by user or automatically);

c) Calculate the updated  $F_{cap}(T_{bat})$  value at temperature  $T_{bat}$  as follows:  $F_{cap}^{(new)}(T_{bat}) = F_{cap}^{(old)}(T_{bat}) + \alpha \cdot \{ \Delta C_{actual} / \Delta C_{est} - F_{cap}^{(old)}(T_{bat}) \}$ ; where  $\alpha$  is a small constant for iterative correction;  $T_{bat}$  is the average temperature between the time issuing the battery low warning message and the time radio is turned off; and  $F_{cap}^{(old)}(T_{bat})$  is the interpolated value on table FCAP\_VS\_T at the temperature  $T_{bat}$  before FCAP\_VS\_T is updated;

d) Update the element FCAP\_VS\_T(n) (340A) by the value  $F_{cap}^{(new)}(T_{bat})$ , where n is the closest element to temperature  $T_{bat}$  in the span of table FCAP\_VS\_T.

If the mobile device 110 has never been operated at a given temperature range, then the corresponding element of RESR\_VS\_T and/or FCAP\_VS\_T will have never been updated.

Thus, the first time the method attempts to retrieve  $F_{esr}(T_{bat})$  and/or  $F_{cap}(T_{bat})$  in that range, the initial value of 1.0 may be inaccurate. If the neighboring elements to the  $F_{cap}(T_{bat})$  value in table FCAP\_VS\_T and to the  $F_{esr}(T_{bat})$  value in table FESR\_VS\_T are not equal to the initial value (1.0), additional processing can reduce the initial error. If only one suitable neighboring element is available at one side of  $F_{esr}(T_{bat})$  or  $F_{cap}(T_{bat})$  and it is significantly different from 1.0, then the neighbor value may be used for  $F_{esr}(T_{bat})$  or  $F_{cap}(T)$  instead of 1.0, otherwise, the value 1.0 may be used. When there are two suitable

neighboring values on either side of  $F_{\text{esr}}(T_{\text{bat}})$  or  $F_{\text{cap}}(T)$ , then a value may be interpolated using the neighboring values for  $F_{\text{esr}}(T_{\text{bat}})$  or  $F_{\text{cap}}(T)$ .

Alternatively, the table  $\text{FCAP\_VS\_T}$  may be reduced to only one element that is not a function of temperature, and corrections to  $\text{CAP\_VS\_V}$  may be made using only the single factor  $F_{\text{cap}}$  for any temperature. In this case, the following equations may be used:

$$C_{\text{user}}(V) = F_{\text{cap}} \cdot C_{\text{model}}(V); \text{ and}$$

$$F_{\text{cap}}^{(\text{new})} = F_{\text{cap}}^{(\text{old})} + \alpha \cdot \{ \Delta C_{\text{actual}} / \Delta C_{\text{est}} - F_{\text{cap}}^{(\text{old})} \}.$$

Fig. 4 is a flowchart of an example method 400 for selecting a battery profile. The method 400 is initiated when a battery pack, such as the battery pack 110 of Fig. 2, is inserted 410. The battery pack is identified at step 420. The identification may, for example, be performed by the identification module 116 of Fig. 2 or, alternatively, by measurement of a characteristic property of the battery pack, such the ESR.

In step 430, the method determines if a profile exists for the battery pack. If a profile is determined to exist, then the existing profile corresponding to the pack is selected at step 440 in response to the predetermined characteristic. Conversely, if no profile exists, then a new profile is created at step 450, as described above. This new profile is then selected at step 460. In either case, after the profile is selected, the process requesting the battery profile resumes at step 470. This method enables multiple profiles, such as profiles 230A-N illustrated in Fig. 3, to be used, each corresponding to one battery pack of the same type or different types.

Fig. 5 is a flowchart that illustrates a method of sampling battery measurements, as described with reference to step 310 of Fig. 3. At step 514, a selection signal, such as that illustrated connecting microprocessor 138 and ADC 250 in Fig. 2, is sent. The value of the measurement is obtained at step 516 by reading the value generated by the ADC. Step 516 determines if all measurements have been read. If not, then the method returns to step 514 with an unprocessed measurement. Otherwise, the method ends at step 520.

Fig. 6 is a flowchart of an example preprocessing method, as described with reference to step 320 of Fig. 3. The battery profile 330 is consulted for a corresponding interpolation table for the ADC value in step 622. If found, the ADC value is interpolated using the corresponding table in step 624. The intermediate results are computed in step 626 based on the linearized measurements obtained from the previous step. Intermediate results, as well as



processing results, are described below with reference to Fig. 7. At step 628, the method determines if all ADC values have been processed. If all ADC values have not been processed, then the method returns to step 622 with an unprocessed ADC value. Otherwise, the method ends at step 630.

Fig. 7 is a flowchart of an example method 700 for measurement, preprocessing, and capacity processing, as described above with reference to Fig. 3. Measurements obtained with the apparatus of Fig. 2 are illustrated by temperature T 710, transmit power TXp 712, measured current I1 714 and loaded battery voltage V\_load 716. It should be understood, however, that although both TXp 712 and I1 714 are illustrated, only one may be required.

At step 718, the ESR\_VS\_T table 332 of profile 330 and T 710 are used to obtain the ESR 720 by interpolation. At step 722, the I\_VS\_TXP table 334 of profile 330 and TXp 712 are used to obtain the current I 724. The current I 724 further includes the I(state) that is determined by the state of other devices, such as a buzzer, backlight and LED. Alternatively, at step 726, if current I1 is available directly, then current I1 714 may be used instead of current I in subsequent processing steps.

At step 730, the FESR\_VS\_T table 342 of profile 330 and T 710 are used to obtain factor F\_esr 732. Alternatively, F\_esr may be a scalar that does not depend on temperature. At step 728, the ESR 720, F\_esr 732 and either current I1 714 or current I 724 are used to obtain the unloaded voltage V 734 according to the equation  $V = V\_load + F\_esr \cdot ESR \cdot (I \text{ or } I1)$ , where (I or I1) signifies that either value of I or I1 can be used in the equation.

At step 736, the CAP\_VS\_V table 338 of profile 330 and V 734 are used to obtain a model capacity C\_model 738 by interpolation.

At step 742, the FCAP\_VS\_T table 340 and T 710 are used to obtain factor F\_cap 744 by interpolation. Alternatively, F\_cap may be a scalar that does not depend on temperature.

At step 740, F\_cap 744 and C\_model 738 are used to determine a capacity to show the user C\_user 750, a first processing result.

At step 746, the table VROFF\_VS\_T 336 of profile 330 and T 710 are used to obtain the radio off threshold voltage VROFF 748, a second result, by interpolation. Note that in Fig. 7, Tbat and Tbrd are both represented by the same symbol T. Alternatively, step 746 may use Tbrd, and all other places use T (i.e., Tbat).

In one alternative embodiment, VROFF might be used instead of V at step 736 as an intermediate step to determine a condition for a capacity based condition-action operation. One such voltage based condition-action operation is described below with reference to Fig. 12.

5        Fig. 8 is a flowchart 800 of an example self-calibration method, as described above with reference to Fig. 3. This method 800 is a continuation of step 734 of Fig. 7.

10        The unloaded voltage V is compared at step 810 to an upper limit threshold, V<sub>upper</sub>, and a lower limit threshold, V<sub>lower</sub>. These limits may, for example, be two unloaded voltage thresholds that are determined based on the battery characterization. For example, V<sub>upper</sub> may be 4.0V and V<sub>lower</sub> may be 3.6V, but other threshold voltages could also be used.

      If the voltage is within the threshold, then the FESR\_VS\_T table 342 is updated at step 820. The method of calibrating the FESR\_VS\_T table 342 is described in more detail with reference to Fig. 9. The normal operation of the mobile device then continues at step 830.

15        Fig. 9 is a flowchart of an example self-calibration method for the FESR\_VS\_T compensation factor described above with reference to Fig. 8. Two circular buffers are created at step 901. One buffer holds the measured current and the other holds the measured battery voltage. For example, each buffer may be 8 bytes long, but other sized buffers could also be used.

20        The values in the buffers are updated at predetermined intervals at step 903. One example of such an interval is every two seconds. The voltage and current samples are collected at substantially the same time and stored in the buffer as new values. The oldest values are discarded.

25        Variables are also created at step 905. These variables may include I<sub>min</sub>, I<sub>max</sub>, V<sub>Imin</sub>, and V<sub>Imax</sub>, where I<sub>min</sub> is the minimum current value within the circular buffer for current after the last update with V<sub>Imin</sub> being the voltage measured at substantially the same time as I<sub>min</sub>. I<sub>max</sub> is the maximum current value within the circular buffer for current after the last update, with V<sub>Imax</sub> being the voltage measured at substantially the same time that I<sub>max</sub> is measured. Alternatively, the current value may be obtained using a table that contains pre-measured current values based on the mobile device's state (e.g., transmit power  
30    high, stand-by mode, vibrator on) at each current value.

At step 910, the variables are updated at the same predetermined intervals as the values in the buffer (e.g., 2 seconds). If  $I_{max} - I_{min}$  is less than a predetermined threshold such as 100 mA, then the method returns to step 903 to update the buffer.

If  $I_{max} - I_{min}$  is greater than the predetermined threshold (e.g., 100 mA), then at step 920 the method finds the estimated ESR and updates the compensation factor for ESR in table FESR\_VS\_T. This step may be accomplished as follows:

$$ESR_{estimate}(T_{bat}) = (V_{I_{min}} - V_{I_{max}}) / (I_{max} - I_{min}),$$

$F_{esr}^{(new)}(T_{bat}) = F_{esr}^{(old)}(T_{bat}) + \beta \cdot \{ ESR_{estimated}(T_{bat}) / ESR(T_{bat}) - F_{esr}^{(old)}(T_{bat}) \}$ ; where  $ESR(T_{bat})$  is the interpolated value at current temperature  $T_{bat}$  (assuming that temperature change is small during 16 seconds) and  $\beta$  is a small constant in the range of 0.01 – 0.30.  $F_{esr}^{(old)}(T_{bat})$  is the interpolated value from the table FESR\_VS\_T at temperature  $T_{bat}$  before the table is updated.

The value of the entry in the table FESR\_VS\_T (342A) of Fig. 3 with a corresponding temperature closest to  $T_{bat}$  is updated by the value  $F_{esr}^{(new)}(T_{bat})$  as described above with respect to the array FESR\_VS\_T. Alternatively, the single element FESR may be updated by  $F_{esr}^{(new)}(T_{bat})$ , as described above.

The circular buffers and variables are reset at 925. The method then repeats from step 901.

Fig. 10 is a flowchart of another example self-calibration method in accordance with Fig. 3. In this method 1000, if a battery low indication is detected at step 1010, then the FCAP\_VS\_T table 340 is updated at step 1020. The normal operation of the mobile device then continues at step 1030. A method of updating the FCAP\_VS\_T table 340 is illustrated in greater detail with reference to Fig. 11.

Fig. 11 is a flowchart of an example method for self-calibration of the compensation factor, FCAP\_VS\_T, as described with reference to Fig. 10. The method begins after a low battery warning message has been generated by the mobile device. An accumulator starts to accumulate values of  $I_{battery}$  at predefined intervals (e.g., 8 seconds) at step 1101.

After step 1101, two scenarios may occur. First, the mobile device user may not terminate the call or other high current application causing the mobile unit to shut off (i.e., the call terminates). Second, the user may terminate the call or other usage after the low battery warning message is given but before the mobile unit shuts off.

In any case, the accumulation stops at step 1105 when the call terminates. The last value of  $\Sigma I_{\text{battery}}$  is determined at step 1110, as described above, and the value is used to calculate the actual capacity drop at step 1115 using the following equation:

$$\Delta C_{\text{actual}} = \Delta t \cdot \Sigma I_{\text{battery}}.$$

5        The model estimated capacity drop before correction,  $C_{\text{est}}$ , is then determined at step 1120 using the equation:

$$\Delta C_{\text{est}} = C_{\text{model}}(V_{\text{warn}}) - C_{\text{model}}(V_{\text{idle}});$$

where  $V_{\text{warn}}$  is the unloaded voltage converted from the loaded voltage at the time the low battery warning message is issued and  $V_{\text{idle}}$  is the unloaded voltage converted from  
10        the loaded voltage obtained immediately after either user termination of the call or the radio shut-off event occurs.

The capacity calibration factor,  $F_{\text{cap}}$ , is calculated at step 1125 and the  $\text{FCAP\_VS\_T}$  updated, as described above.

Fig. 12 is a flowchart illustrating an example warning action during a call. This  
15        method 1000 may, for example, begin from step 734 of Fig. 7. A “battery low” warning message may be presented on the mobile unit display or by an aural tone in response to the first occurrence of the following event:

$$C_{\text{user}}(V, T_{\text{bat}}) - C_{\text{user}}(V_{\text{ROFF\_unload}}, T_{\text{bat}}) < I_{\text{battery}} \cdot t_0;$$

where  $t_0$  is a predefined time advance before radio shut off (e.g., 4 minutes),  $V$  is the  
20        unloaded voltage translated from measured loaded voltage value described above with reference to step 320) in Fig. 3,  $T_{\text{bat}}$  is the measured temperature for battery,  $I_{\text{battery}}$  is the battery current calculated from the table of step 320 of Fig. 3,  $V_{\text{ROFF\_unload}}$  is the unloaded voltage translated by loaded voltage threshold value calculated in step 320 of Fig. 3. The translation is given as:

$$25 \quad V_{\text{ROFF\_unload}} = V_{\text{ROFF}}(T_{\text{brd}}) + I_{\text{battery}} \cdot F_{\text{esr}}(T_{\text{bat}}) \cdot \text{ESR}(T_{\text{bat}}).$$

The method of Fig. 12 determines if the estimated battery capacity is less than the predetermined threshold at step 1210 (i.e.,  $I_{\text{battery}} \cdot t_0$ ). If the left hand side, determined by  $V$ , has not crossed below the threshold, then the mobile device’s normal operation continues at step 1230. If the left hand side, determined by  $V$ , goes below the threshold at step 1210, then  
30        a series of condition-action operations are initiated at step 1220. The actions triggered at step 1220 include issuing a warning such as an audible beep and/or a message displayed on screen,

and starting the FCAP\_VS\_T self calibration, as described above. The normal operation of the mobile device then continues at step 1230.

Additionally, a mobile device shut-off is triggered by the first occurrence of:

$V_{load\_this\_time} < V_{ROFF}(T_{brd\_this\_time});$

5        where  $V_{load\_this\_time}$  is the voltage measured any time after the “battery low” warning,  $T_{brd\_this\_time}$  is the temperature measured at the same time that  $V_{load\_this\_time}$  is measured, after the “battery low” warning, and  $V_{ROFF}()$  uses the threshold table for radio shut-off given by the results of step 320 in Fig 3.

10        The battery charge current estimation method may, for example, use the estimated battery ESR and unloaded voltage in conjunction with measuring the battery terminal voltage in both the charger on state and the charger off state.

Battery charge current is estimated by first measuring the battery terminal voltage while charging ( $V_{charge}$ ). The charger is then disabled for a short period of time to allow the unloaded battery voltage to be estimated as described above.

15        The unloaded voltage ( $V(T_{bat})$ ) and the battery terminal voltage during charging ( $V_{charge}$ ) may be used to estimate the charge current as  $I_{chg} = (V_{charge} - V(T_{bat})) / (F_{esr}(T_{bat}) * ESR(T_{bat}))$ .

20        This written description uses examples to disclose the invention, including the best made, and also to enable a person skilled in the art to make and use the invention. The patentable scope of the invention may include other examples that occur to those skilled in the art. For example, the examples described above refer to mobile communication devices. However, other electronic device requiring batteries for operation may also benefit from the technology described herein.